

## ESTIMATING RUNOFF VOLUME = ROCKET SCIENCE



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### Why Runoff Volume?

- Many stormwater programs have a volume control requirement; that is, capturing the first 1 or 1.5 inches of stormwater and retaining it for 2 to 5 days.
- Similarly, Erosion Control measures are required to capture a volume and discharge it over a 2 to 5 day period.

### Hydrologic Components

- Watershed Characteristics – Drainage Area, Land Use, Types of Soil, and Time of Concentration.
- Storm Characteristics – Type, Duration, Total Volume, Intensity, and Distribution.

### SELECTING THE RIGHT METHOD!

- Acceptable methods to calculate peak discharge.
  1. Rational Method
  2. NRCS, TR-55 Graphical Peak Flow Method (also known as the SCS Method)
- Which method do I use?
  1. Rational Method: drainage area is less than 50 acres
  2. SCS Method: drainage area is greater than 20 acres, also the SCS method should only be used when the Curve Number exceeds 50 and the time of concentration is greater than 0.1 hr and less than 10 hr.

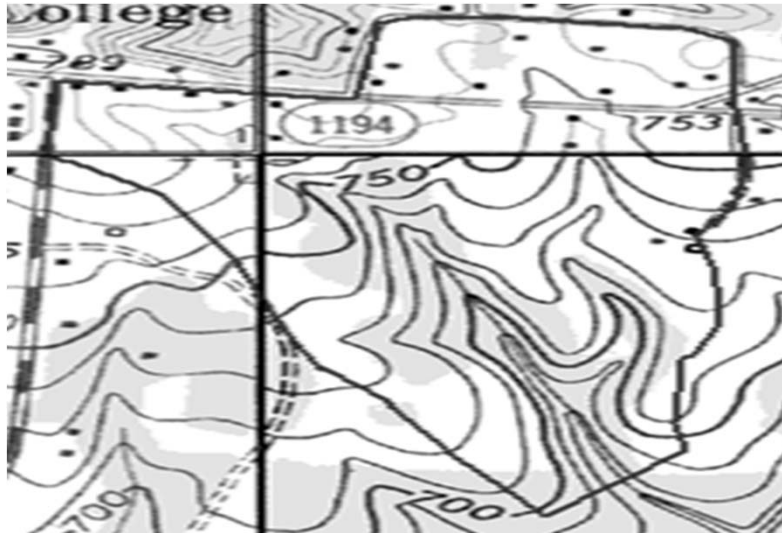
## USING THE NRCS METHOD

- Step 1. Determine the drainage area.
- Step 2. Determine a weighted Curve Number and Tc
- Step 3. Select appropriate Rainfall amounts. (Depth, not intensity)
- Step 4. Determine peak discharge.

## Example #1

- Using the SCS Method, determine the total amount of runoff volume produced from a 10 year storm event that is located in Boone, NC. Two-thirds of the site is to be cleared and graded, while one-third will be left alone as dense woods.
- Drainage area of 45 acres
- Assume all soils are Hydrologic Group B
- The time of concentration:
  - Sheet flow of 50' with a slope of 8% made of Dense Woods.
  - Shallow concentrated flow of 250' with a slope of 6.5% unpaved.
  - Channel flow of 450' with a slope of 3.5% using a bankfull flow area of 4.5 ft<sup>2</sup> and a wetted perimeter of 5.0'. (Use n = 0.055)
- <http://websoilsurvey.nrcs.usda.gov/app/HomePage.htm>

# Hydrologic Components



# NRCS SOIL WEB SURVEY

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- APDTG
- National Soil Characterization Data
- Soil Geochemistry Spatial Database
- Soil Quality
- Soil Geography

The simple yet powerful way to access and use soil data.

**START WSS**

**Welcome to Web Soil Survey (WSS)**

Web Soil Survey (WSS) provides soil data and information produced by the National Cooperative Soil Survey. It is operated by the USDA Natural Resources Conservation Service (NRCS) and provides access to the largest natural resource information system in the world. NRCS has soil maps and data available online for more than 95 percent of the nation's counties and anticipates having 100 percent in the near future. The site is updated and maintained online as the single authoritative source of soil survey information.

**Three Basic Steps**

- 1 Define... Use the Area of Interest tab to define your area of interest.

**Area of Interest (AOI)**

I Want To...

- Start Web Soil Survey (WSS)
- Know the requirements for running Web Soil Survey
- Know whether Web Soil Survey works in my web browser
- Know the Web Soil Survey hours of operation
- Find what areas of the U.S. have soil data

Announcements/Events

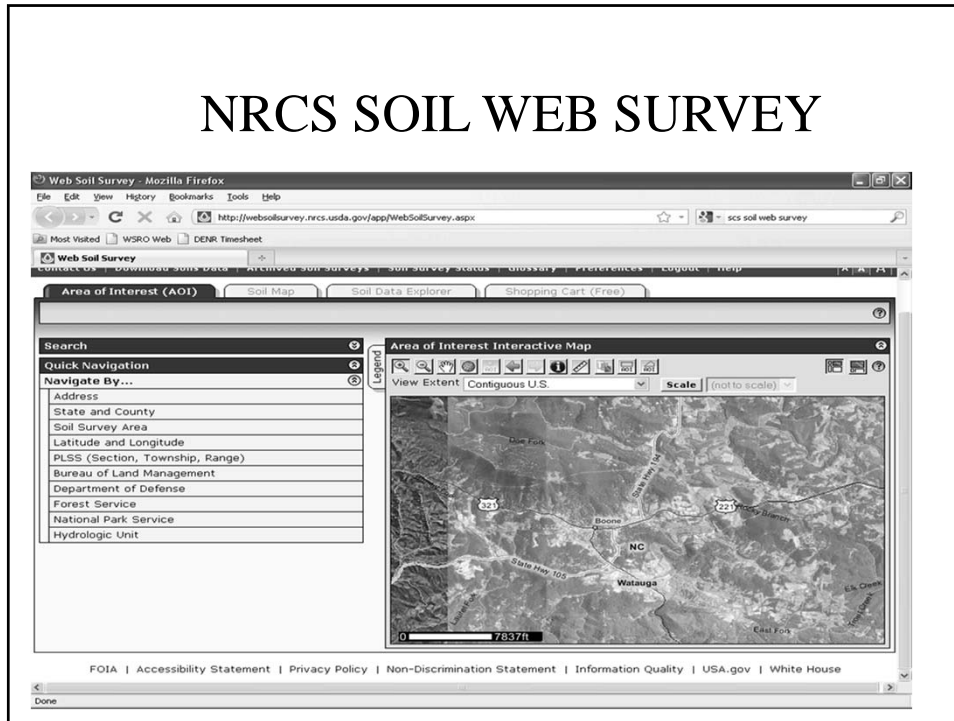
- Web Soil Survey Release History

I Want Help With...

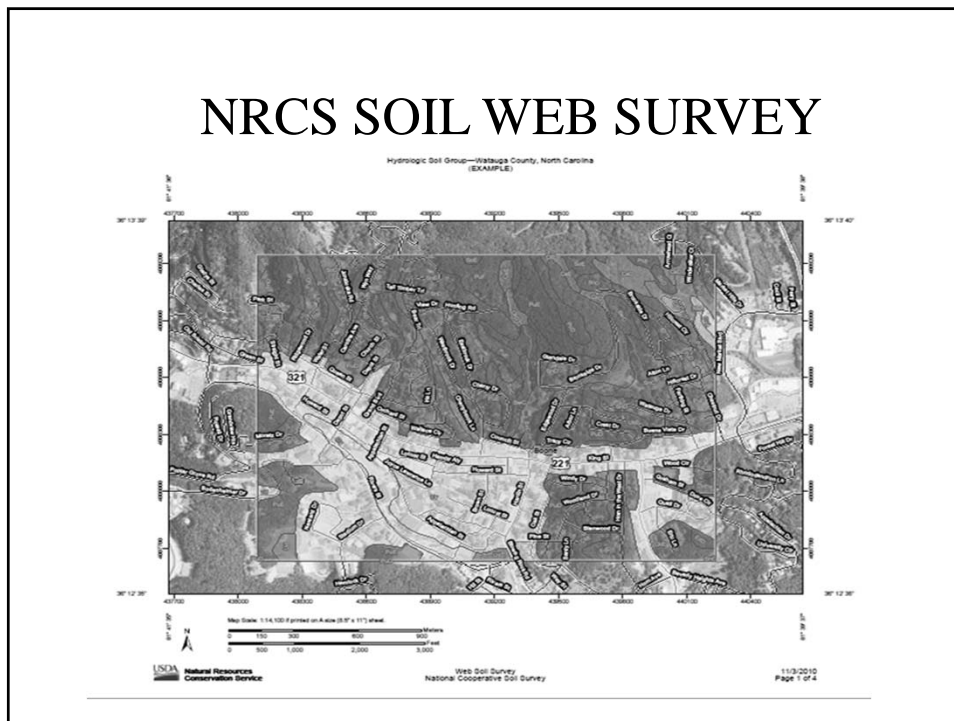
- How to use Web Soil Survey
- How to use Web Soil Survey Online Help
- Known Problems and Workarounds
- Frequently Asked Questions
- Citing Web Soil Survey as a source of soil data

Transferring data from websurvey.nrcs.usda.gov...

# NRCS SOIL WEB SURVEY



# NRCS SOIL WEB SURVEY



## Four Hydrologic Soil Groups as Defined by the SCS (1986)

Group A - A soils have low runoff potential and high infiltration rates and have a high rate of water transmission (greater than 0.30 in/hr). The textures of these soils are typically sand, loamy sand, or sandy loam.

Group B - B soils have moderate infiltration rates and have a moderate rate of water transmission (0.15-0.30 in/hr). The textures of these soils are typically silt loam or loam.

Group C - C soils have low infiltration rates and have a low rate of water transmission (0.05-0.15 in/hr). The texture of these soils is typically sandy clay loam.

Group D - D soils have high runoff potential and have a very low rate of water transmission (0-0.05 in/hr). The textures of these soils are typically clay loam, silty clay loam, sandy clay, silty clay, or clay.

## NRCS SOIL WEB SURVEY

RUSLE2 Related Attributes—Iredell County, North Carolina								
Map symbol and soil name	Pct. of map unit	Slope length (ft)	Hydrologic group	Kf	T factor	Representative value		
						% Sand	% Silt	% Clay
ToC2—Tomlin sandy clay loam, 6 to 10 percent slopes, moderately eroded								
Tomlin, moderately eroded	90	230	B	.10	5	55.1	14.9	30.0
ToD2—Tomlin sandy clay loam, 10 to 15 percent slopes, moderately eroded								
Tomlin, moderately eroded	80	—	B	.10	5	55.1	14.9	30.0
ToE2—Tomlin sandy clay loam, 15 to 25 percent slopes, moderately eroded								
Tomlin, moderately eroded	80	—	B	.10	5	55.1	14.9	30.0

### Data Source Information

Soil Survey Area: Iredell County, North Carolina  
 Survey Area Data: Version 18, Jul 6, 2012

**Table 8.03e Runoff curve numbers of urban areas<sup>1</sup>**

Cover Description		Curve number for hydrologic soil group			
Cover type and hydrologic condition	Average percent impervious area <sup>2</sup>	A	B	C	D
<i>Fully developed urban areas (vegetation established)</i>					
Open space (lawns, parks, golf courses, cemeteries, etc.) <sup>3</sup> :					
Poor condition (grass cover < 50%) .....		68	79	86	89
Fair condition (grass cover 50% to 75%) .....		49	69	79	84
Good condition (grass cover > 75%) .....		39	61	74	80
Impervious areas:					
Paved parking lots, roofs, driveways, etc. (excluding right-of-way) .....		98	98	98	98
Streets and roads:					
Paved; curbs and storm sewers (excluding right-of-way) .....		98	98	98	98
Paved; open ditches (including right-of-way) .....		83	89	92	93
Gravel (including right-of-way) .....		76	85	89	91
Dirt (including right-of-way) .....		72	82	87	89
Urban districts:					
Commercial and business .....	85	89	92	94	95
Industrial .....	72	81	88	91	93
Residential districts by average lot size:					
1/8 acre or less (town houses) .....	65	77	85	90	92
1/4 acre .....	38	61	75	83	87
1/3 acre .....	30	57	72	81	86
1/2 acre .....	25	54	70	80	85
1 acre .....	20	51	68	79	84
2 acres .....	12	46	65	77	82
<i>Developing urban areas</i>					
Newly graded areas (pervious areas only, no vegetation) <sup>4</sup> .....		77	86	91	94
Idle lands (CN's are determined using cover types similar to those in table 2-2c).					

**Table 8.03g Runoff curve numbers for other agriculture lands<sup>1</sup>**

Cover description		Curve numbers for hydrologic soil groups			
Cover type	Hydrologic conditions <sup>3</sup>	A	B	C	D
Pasture, grassland, or range—continuous forage for grazing. <sup>2</sup>	Poor	68	79	86	89
	Fair	49	69	79	84
	Good	39	61	74	80
Meadow—continuous grass, protected from grazing and generally mowed for hay.	—	30	58	71	78
Brush—brush-weed-grass mixture with brush the major element. <sup>3</sup>	Poor	48	67	77	83
	Fair	35	56	70	77
	Good	30 <sup>4</sup>	48	65	73
Woods—grass combination (orchard or tree farm). <sup>5</sup>	Poor	57	73	82	86
	Fair	43	65	76	82
	Good	32	58	72	79
Woods. <sup>6</sup>	Poor	45	66	77	83
	Fair	36	60	73	79
	Good	30 <sup>4</sup>	55	70	77
Farmsteads—buildings, lanes, driveways, and surrounding lots.	—	59	74	82	86

## LAND USE

- Total Drainage area = 45 acres
  - $(2/3) * 45 = 30$  acres cleared
  - $(1/3) * 45 = 15$  acres dense woods
  
- CN Values (These values can be found in the Manual, Chapter 8.)
- CN = 86 for Newly Graded Areas
- CN = 55 for Dense Woods
  
- Weighted CN-Value
- $CN * A = (86) * (30 \text{ ac}) + (55) * (15 \text{ ac}) = 3405$  (Divide by total Acreage)
- Weighted CN-Value =  $\sum CN * A / A_T \gg \gg 3405 / 45 = 75.67$

## TR-55

MBPOLING

Spring Workshop  
NRCS Method  
Wake County, North Carolina

### Sub-Area Land Use and Curve Number Details

Sub-Area Identifier	Land Use	Hydrologic Soil Group	Sub-Area Area (ac)	Curve Number
Basin #1	Newly graded area (pervious only)	B	30	86
	Woods	(good) B	15	55
Total Area / Weighted Curve Number			45	76
			==	==

The curve number, CN, describes the characteristics of the drainage area that determines the amount of runoff generated by a given storm: hydrologic soil group and groundcover. Soils are classified into four hydrologic soil groups (A, B, C, and D) based on their minimum infiltration rate, with A having the highest infiltration potential and D having the lowest.



*Appendices*

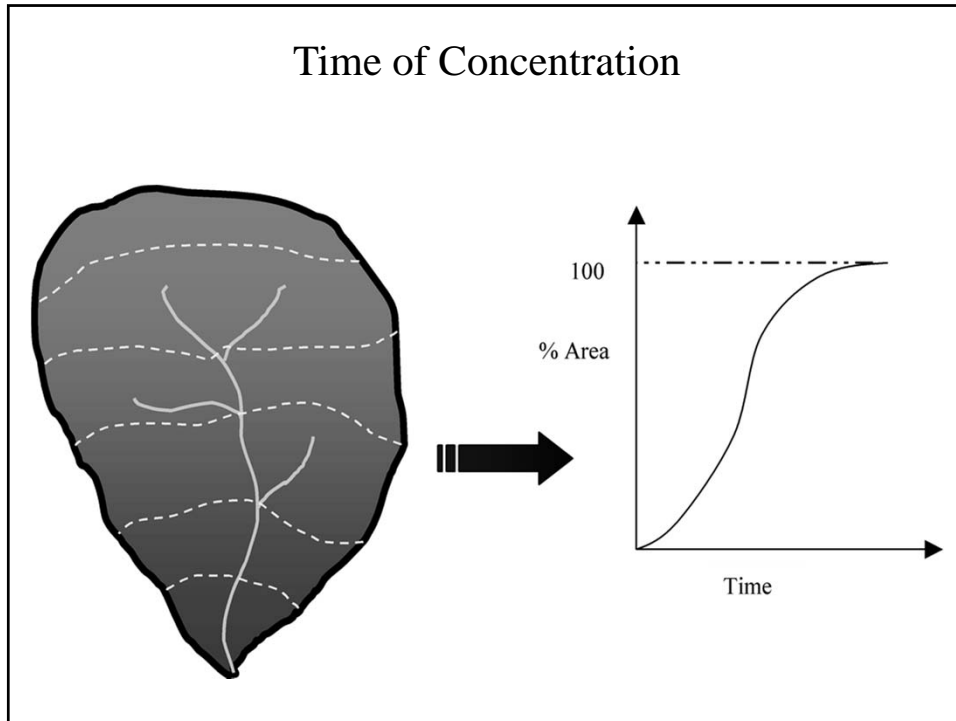
**Worksheet 1: Runoff curve number and runoff**

Project _____		By _____		Date _____	
Location _____		Checked _____		Date _____	
Check one: <input type="checkbox"/> Present <input type="checkbox"/> Developed					
<b>1. Runoff curve number</b>					
Soil name and hydrologic group	Cover description <small>(soil type, treatment, and hydrologic condition; percent impervious, unconnected/connected impervious area ratio)</small>	CN <sup>1</sup>		Area	Product of CN x area
		Table 8.03a	Figure 8.03c	<input type="checkbox"/> acres <input type="checkbox"/> m <sup>2</sup> <input type="checkbox"/> %	
1. Use only one CN source per line.		Totals			
CN (weighted) = $\frac{\text{total product}}{\text{total area}}$ = _____				Use CN <input type="checkbox"/>	
<b>2. Runoff</b>					
Frequency _____ yr		Storm #1	Storm #2	Storm #3	
Rainfall, P (24-hr) _____ in					
Runoff, Q _____ in					
<small>(Use P and CN with table 8.03a, figure 8.03c, or equations 8.03b and 8.03d)</small>					

Rev. 6/94 8.03.25

## Hydrologic Components

- **Time of concentration** is a concept used in hydrology to measure the response of a watershed to a rain event. It is defined as the time needed for water to flow from the most remote point in a watershed to the watershed outlet. It is a function of the topography, geology, and land use within the watershed. (Wikipedia)
- $t_c = t_{\text{sheet}} + t_{\text{shallow}} + t_{\text{channel}}$



**Worksheet 2: Time of Concentration ( $T_c$ ) or travel time ( $T_t$ )**

Project _____	By _____	Date _____
Location _____	Checked _____	Date _____

Check one:  Present  Developed  
 Check one:   $T_c$    $T_t$  through subarea  
 Note: Space for as many as two segments per flow can be used for each worksheet. Include a map, schematic, or description of flow segments.

---

**Sheet flow (Applicable to  $T_c$  only)**

Segment ID: \_\_\_\_\_

- Surface description (table 8.03h) \_\_\_\_\_
- Manning's roughness coefficient,  $n$  (table 8.03h) \_\_\_\_\_
- Flow length,  $L$  (total  $L + 300ft$ ) \_\_\_\_\_ ft
- Two-year 24-hour rainfall,  $P_2$  \_\_\_\_\_ in
- Land slope,  $s$  \_\_\_\_\_ ft/ft
- $T_t = \frac{0.007 (nL)^2}{P_2^{0.48}}$  Compute  $T_t$  \_\_\_\_\_ hr

+ \_\_\_\_\_ = \_\_\_\_\_

---

**Shallow concentrated flow**

Segment ID: \_\_\_\_\_

- Surface description (paved or unpaved) \_\_\_\_\_
- Flow length,  $L$  \_\_\_\_\_ ft
- Watercourse slope,  $s$  \_\_\_\_\_ ft/ft
- Average velocity,  $V$  (figure 3-1) \_\_\_\_\_ ft/s
- $T_t = \frac{L}{3600 V}$  Compute  $T_t$  \_\_\_\_\_ hr

+ \_\_\_\_\_ = \_\_\_\_\_

---

**Channel flow**

Segment ID: \_\_\_\_\_

- Cross sectional flow area,  $a$  \_\_\_\_\_ ft<sup>2</sup>
- Wetted perimeter,  $P_w$  \_\_\_\_\_ ft
- Hydraulic radius,  $r = \frac{a}{P_w}$  Compute  $r$  \_\_\_\_\_ ft
- Channel slope,  $s$  \_\_\_\_\_ ft/ft
- Manning's roughness coefficient,  $n$  \_\_\_\_\_
- $V = \frac{1.49 r^{4/3} s^{1/2}}{n}$  Compute  $V$  \_\_\_\_\_ ft/s
- Flow length,  $L$  \_\_\_\_\_ ft
- $T_t = \frac{L}{3600 V}$  Compute  $T_t$  \_\_\_\_\_ hr
- Watershed or subarea or (add in step 6,11, and 19) \_\_\_\_\_ Hr

+ \_\_\_\_\_ = \_\_\_\_\_

Rev. 4/88 8.03.33

# TIME OF CONCENTRATION TR-55

Tc Time of Concentration Details
⌵ ⌵ ⌵

Sub-area Name  
Watershed
Rename
Clear

2-Year Rainfall (in)  
4.39

### Time of Concentration Details

Flow Type	Length (ft)	Slope (ft/ft)	Surface (Manning's n)	n	Area (ft <sup>2</sup> )	WP (ft)	Velocity (f/s)	Time (hr)
Sheet	50	0.0800	Woods, Dense (0.80)					0.176
Shallow Concentrated	250	0.0650	Unpaved					0.017
Shallow Concentrated								
Channel	450	0.0350		0.055	4.50	5.00	4.808	0.026
Channel								
<b>Total</b>	<b>750</b>						0.9513	<b>0.219</b>

?
Help
Cancel
Accept

File: C:\Documents and Settings\mpoling\Desktop\Presentation.w55 10/15/2010 11:01 AM

~ 13.14 Minutes

# RAINFALL

<b>Boone, North Carolina 36.2167N, 81.6667W</b>										
ARI* (years)	5 min.	10 min.	15 min.	30 min.	60 min.	120 min.	3 hr.	6 hr.	12 hr.	24 hr.
2	0.48	0.76	0.96	1.32	1.66	2.00	2.18	2.85	3.77	4.39
10	0.62	1.00	1.26	1.83	2.39	2.92	3.18	4.10	5.28	6.61
25	0.72	1.14	1.45	2.14	2.85	3.55	3.87	4.94	6.21	8.07
100	0.86	1.38	1.74	2.66	3.67	4.69	5.15	6.47	7.82	10.65

## SCS Peak Discharge Method

- $Q = \frac{(P-0.2S)^2}{(P+0.8S)}$
- $Q =$  Depth of Runoff (in) over the entire watershed.
- $P =$  Rainfall (Depth in inches of a 24 hour event)
- $S =$  Potential maximum retention after run off begins (in)
- $S = \frac{1000}{CN} - 10$ ;  $S = 3.22$
- $Q = \frac{(6.61 - (0.2*3.22))^2}{(6.61 + (0.8*3.22))}$ ;  $Q = 3.88$  Inches of Runoff

## Graphical Peak Discharge Method

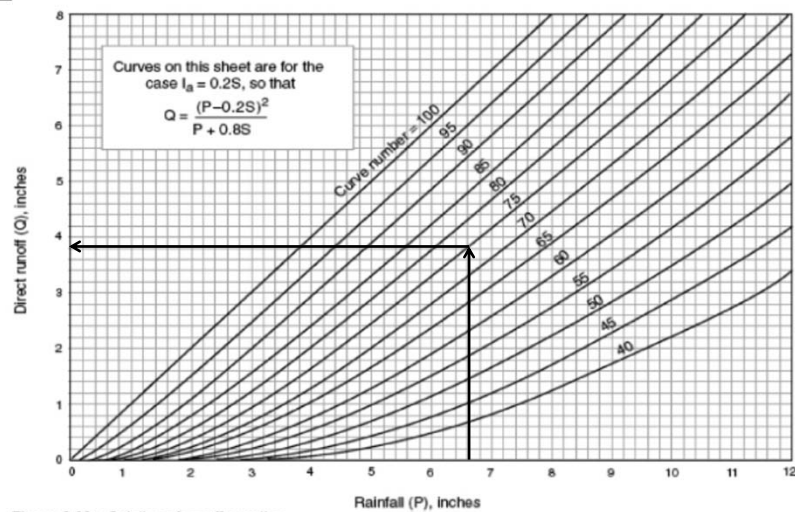


Table 8.03d Runoff depth for selected CN's and rainfall amounts <sup>1</sup>

Rainfall	Runoff depth for curve number of—													
	40	45	50	55	60	65	70	75	80	85	90	95	98	
	inches													
1.0	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.03	0.08	0.17	0.32	0.56	0.79
1.2	0.00	0.00	0.00	0.00	0.00	0.00	0.00	.03	.07	.15	.27	.46	.74	.99
1.4	0.00	0.00	0.00	0.00	0.00	0.02	.06	.13	.24	.39	.61	.92	1.18	1.38
1.6	0.00	0.00	0.00	0.00	0.01	.05	.11	.20	.34	.52	.76	1.11	1.38	1.58
1.8	0.00	0.00	0.00	0.00	.03	.09	.17	.29	.44	.65	.93	1.29	1.58	1.77
2.0	0.00	0.00	0.00	.02	.06	.14	.24	.38	.56	.80	1.09	1.48	1.77	1.96
2.5	0.00	0.00	.02	.08	.17	.30	.46	.65	.89	1.18	1.53	1.96	2.27	2.45
3.0	0.00	.02	.09	.19	.33	.51	.71	.96	1.25	1.59	1.98	2.45	2.77	2.94
3.5	.02	.08	.20	.35	.53	.75	1.01	1.30	1.64	2.02	2.45	2.94	3.27	3.42
4.0	.06	.18	.33	.53	.76	1.03	1.33	1.67	2.04	2.46	2.92	3.43	3.77	3.92
4.5	.14	.30	.50	.74	1.02	1.33	1.67	2.05	2.46	2.91	3.40	3.92	4.26	4.42
5.0	.24	.44	.69	.98	1.30	1.65	2.04	2.45	2.89	3.37	3.88	4.42	4.76	4.96
6.0	.50	.80	1.14	1.52	1.92	2.35	2.81	3.28	3.76	4.30	4.85	5.41	5.76	5.96
7.0	.84	1.24	1.68	2.12	2.60	3.10	3.62	4.15	4.69	5.25	5.82	6.41	6.76	6.96
8.0	1.25	1.74	2.25	2.78	3.33	3.89	4.46	5.04	5.63	6.21	6.81	7.40	7.76	7.96
9.0	1.71	2.29	2.88	3.49	4.10	4.72	5.33	5.95	6.57	7.18	7.79	8.40	8.76	8.96
10.0	2.23	2.89	3.56	4.23	4.90	5.56	6.22	6.88	7.52	8.16	8.78	9.40	9.76	9.96
11.0	2.78	3.52	4.26	5.00	5.72	6.43	7.13	7.81	8.48	9.13	9.77	10.39	10.76	10.96
12.0	3.38	4.19	5.00	5.79	6.56	7.32	8.05	8.76	9.45	10.11	10.76	11.39	11.76	11.96
13.0	4.00	4.89	5.76	6.61	7.42	8.21	8.98	9.71	10.42	11.10	11.76	12.39	12.76	12.96
14.0	4.65	5.62	6.55	7.44	8.30	9.12	9.91	10.67	11.39	12.08	12.75	13.39	13.76	13.96
15.0	5.33	6.36	7.35	8.29	9.19	10.04	10.85	11.63	12.37	13.07	13.74	14.39	14.76	14.96

<sup>1</sup> / Interpolate the values shown to obtain runoff depths for CN's or rainfall amounts not shown.

## SCS Peak Discharge Method

- Peak Discharge ( $Q_p$ ) =  $q_u * A_m * F_p * Q = \text{CFS}$
- Unit Peak Discharge ( $q_u$ ) From figure 8.03k in the sediment manual (CFS / Square Mile per Inch of Rainfall)
- Drainage Area ( $A_m$ ) =  $\text{mi}^2$
- Pond and Swamp Factor ( $F_p$ ) = 1.0 ~ 0%
- Runoff ( $Q$ ) = Depth in inches

## INITIAL ABSTRACTION

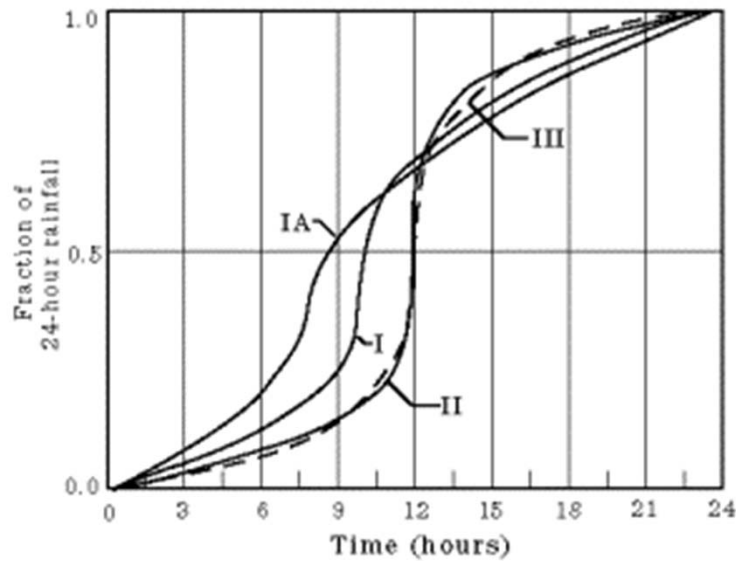
Curve number	$I_a$ (in)	Curve number	$I_a$ (in)
40	3.000	70	0.857
41	2.878	71	0.817
42	2.762	72	0.778
43	2.651	73	0.740
44	2.545	74	0.703
45	2.444	75	0.667
46	2.348	76	0.632
47	2.255	77	0.597
48	2.167	78	0.564
49	2.082	79	0.532
50	2.000	80	0.500

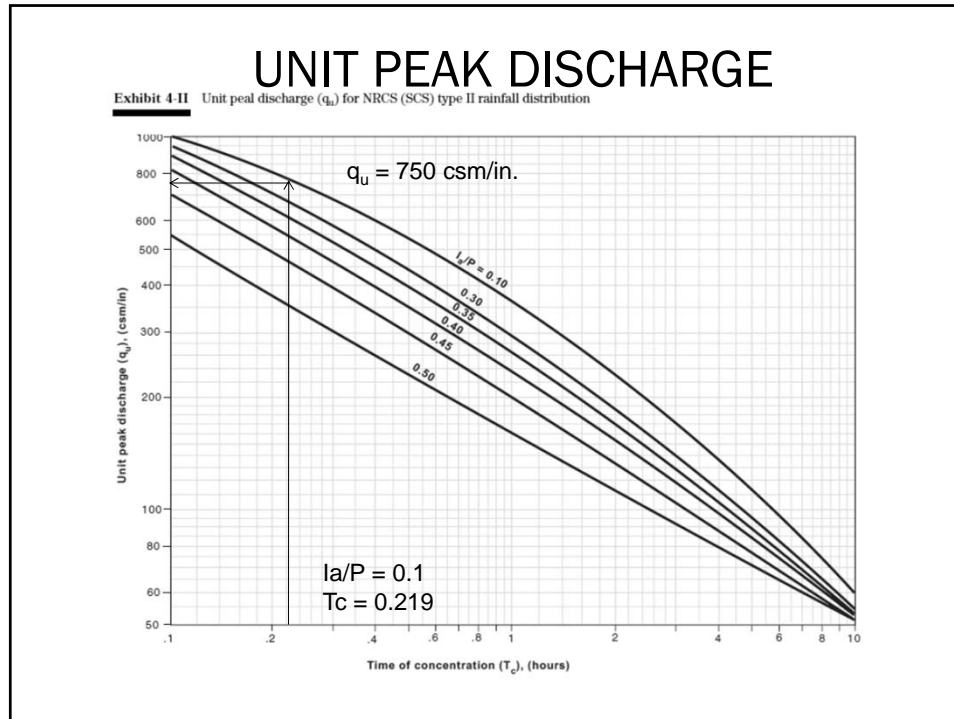
→ CN = 75.67

- Average ( $I_a$ ) = 0.65"
- $I_a/P = 0.65 / 6.61 = 0.1$

Initial abstraction ( $I_a$ ) is all losses before runoff begins. It includes water retained in surface depressions, water being intercepted by vegetation, evaporation, and infiltration.

## Unit Hydrograph





## SCS Peak Discharge Method

- Peak Discharge ( $Q_p$ ) =  $q_u * A_m * F_p * Q = \text{CFS}$
- Unit Peak Discharge ( $q_u$ ) = 350 csm/in (figure 8.03k in the sediment manual) (CFS / Square Mile per Inch of Rainfall)
- Drainage Area ( $A_m$ ) = 45 Acres/640 ac/mi<sup>2</sup> = 0.07 mi<sup>2</sup>
- Pond and Swamp Factor ( $F_p$ ) = 1.0 ~ 0%
- Runoff ( $Q$ ) = 3.88 inches
  
- $Q_p = 750 * 0.07 * 1.0 * 3.88 = 204 \text{ cfs}$

WinTR-55 Main Window

File Options ProjectData GlobalData Run Help

WinTR-55 Small Watershed Hydrology

Project Identification Data

User: MBPOLING State: North Carolina

Project: Spring Workshop County: Wake

Subtitle: NRCS Method Execution Date: 2/25/2014

Sub-areas are expressed in:  Acres  Square Miles

Dimensionless Unit Hydrograph: <standard>

Storm Data Source: User-provided custom storm data

Rainfall Distribution Identifier: Type II

Sub-area Entry and Summary

Sub-area Name	Sub-area Description	Sub-area Flows to Reach/Outlet	Area (ac)	Weighted CN	Tc (hr)
Basin #1		Outlet	45.00	76	0.219

Project Area: 45 (ac)

MBPOLING Spring Workshop  
NRCS Method  
Wake County, North Carolina

Hydrograph Peak/Peak Time Table

Sub-Area or Reach Identifier Peak Flow and Peak Time (hr) by Rainfall Return Period  
10-Yr (cfs) (hr)

-----

SUBAREAS  
Basin #1 227.48  
12.03

REACHES  
OUTLET 227.48



8

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**Worksheet 3: Graphical Peak Discharge Method**

Project	By	Date
Location	Checked	Date

Check one:  Present  Developed

1. Data

Drainage area \_\_\_\_\_  $A_d =$  \_\_\_\_\_  $m^2$  (acres/540)

Runoff curve number \_\_\_\_\_ CN = \_\_\_\_\_ (From worksheet 1)

Time of concentration \_\_\_\_\_  $T_c =$  \_\_\_\_\_ hr (from worksheet 2)

Rainfall disturbance \_\_\_\_\_ = \_\_\_\_\_ (I, IA, II, III)

Pond and swamp areas spread throughout watershed \_\_\_\_\_ = \_\_\_\_\_ percent of  $A_d$  (\_\_\_\_\_ acres or  $m^2$  covered)

2. Frequency \_\_\_\_\_ yr

3. Rainfall, P (24-hour) \_\_\_\_\_ in

4. Initial abstraction,  $I_a$  \_\_\_\_\_ in  
(Use CN with table 8.03h)

5. Compute  $I_a/P$  \_\_\_\_\_

6. Unit peak discharge,  $q_u$  \_\_\_\_\_ cm/in  
(Use  $T_c$  and  $I_a/P$  with figure 8.03k)

7. Runoff, Q \_\_\_\_\_ in  
(From worksheet 1) Figure 8.03e

8. Pond and swamp adjustment factor,  $F_p$  \_\_\_\_\_  
(Use percent pond and swamp area with table 8.03. Factor is 1.0 for zero percent pond and swamp area.)

9. Peak discharge,  $q_p$  \_\_\_\_\_ ft/s  
(Where  $q_p = q_u A_d F_p$ )

	Storm #1	Storm #2	Storm #3
2. Frequency			
3. Rainfall, P (24-hour)			
4. Initial abstraction, $I_a$			
5. Compute $I_a/P$			
6. Unit peak discharge, $q_u$			
7. Runoff, Q			
8. Pond and swamp adjustment factor, $F_p$			
9. Peak discharge, $q_p$			

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## RUNOFF VOLUME

- $Q = 3.88$  Inches of Runoff
- Area = 45 Acres
- Volume = Depth x Area
- Volume = 627,264 Cubic Feet of Runoff
- Volume = 14.4 ac-ft

## EXAMPLE #2

- Using the Rational Method in conjunction with the SCS Triangular Unit Hydrograph Method, determine the total amount of runoff volume produced from a 10 year storm event. Two-thirds of the site is to be cleared and graded, while one-third will be left alone as dense woods.
- Drainage area of 45 acres
- Weighted Runoff Coefficient
- The time of concentration:
  - Sheet flow of 50' with a slope of 8% made of Dense Woods.
  - Shallow concentrated flow of 250' with a slope of 6.5% unpaved.
  - Channel flow of 450' with a slope of 3.5% using a bankfull flow area of 4.5 ft<sup>2</sup> and a wetted perimeter of 5.0'. (Use  $n = 0.055$ )

## RATIONAL METHOD

- Step 1. Determine the Land Use "C" Values.
- Step 2. Determine your time of concentration, time to peak, and time of base.
- Step 3. Select Appropriate Storm

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**Table 8.03b**  
Value of Runoff Coefficient  
(C) for Rational Formula

Land Use	C	Land Use	C
Business:		Lawns:	
Downtown areas	0.70-0.95	Sandy soil, flat, 2%	0.05-0.10
Neighborhood areas	0.50-0.70	Sandy soil, ave., 2-7%	0.10-0.15
Residential:		Sandy soil, steep, 7%	0.15-0.20
Single-family areas	0.30-0.50	Heavy soil, flat, 2%	0.13-0.17
Multi units, detached	0.40-0.60	Heavy soil, ave., 2-7%	0.18-0.22
Multi units, Attached	0.60-0.75	Heavy soil, steep, 7%	0.25-0.35
Suburban	0.25-0.40	Agricultural land:	
Industrial:		Bare packed soil	
Light areas	0.50-0.80	Smooth	0.30-0.60
Heavy areas	0.60-0.90	Rough	0.20-0.50
Parks, cemeteries	0.10-0.25	Cultivated rows	
Playgrounds	0.20-0.35	Heavy soil no crop	0.30-0.60
Railroad yard areas	0.20-0.40	Heavy soil with crop	0.20-0.50
Unimproved areas	0.10-0.30	Sandy soil no crop	0.20-0.40
Streets:		Sandy soil with crop	0.10-0.25
Asphalt	0.70-0.95	Pasture	
Concrete	0.80-0.95	Heavy soil	0.15-0.45
Brick	0.70-0.85	Sandy soil	0.05-0.25
Drives and walks	0.75-0.85	Woodlands	0.05-0.25
Roofs	0.75-0.85		

NOTE: The designer must use judgement to select the appropriate C value within the range for the appropriate land use. Generally, larger areas with permeable soils, flat slopes, and dense vegetation should have lowest C values. Smaller areas with slowly permeable soils, steep slopes, and sparse vegetation should be assigned highest C values.

Source: American Society of Civil Engineers

## LAND USE

- Total Drainage area = 45 acres
  - $(2/3) * 45 = 30$  acres cleared
  - $(1/3) * 45 = 15$  acres dense woods
- C Values (These values can be found in the Manual, Chapter 8.)
- C = 0.6 for Newly Graded Areas
- C = 0.25 for Dense Woods
- Weighted CN-Value
- $CN * A = (0.6) * (30 \text{ ac}) + (0.25) * (15 \text{ ac}) = 21.8$  (Divide by total Acreage)
- Weighted CN-Value =  $\sum CN * A / A_T \gg \gg 21.8 / 45 = 0.48$

## Time of Concentration and the Jarrett Method

- Jarrett (2005) determined that the time of concentration,  $t_c$ , is approximated as 5 minutes for watersheds smaller than the Jarrett Maximum Area.

## Jarrett Method for Small Drainage Areas

- $A_{\text{jarrett}} = \text{Jarrett Maximum Area (ac)}$ 
  - $A_{\text{jarrett}} = 460 * (S)$
- $S = H / L$ 
  - $S = \text{Average Slope Length (ft)}$
  - $H = \text{Change in Elevation (ft)}$
  - $L = \text{Flow Length (ft)}$

## Jarrett Method for Small Drainage Areas

- Drainage Area = 45 acres
- $A_{\text{jarrett}} = 460 * (S)$ 
  - $S = 0.048 \text{ ft/ft}$
- $A_{\text{jarrett}} = 460 * (0.048) = 22.08$
- $45 > 22.08$  Therefore cannot assume 5 minute time of concentration

## TIME OF CONCENTRATION

The Kinematic Wave Theory

SOLVED THROUGH ITERATIONS

$$T_C = \frac{\left[ \frac{L}{\left( \frac{1.49 * S^{1/2}}{n} \right) \left( \frac{I_i * C}{43,200} \right)^{2/3}} \right]^{3/5}}{60}$$

where:

L = length of overland flow plane (feet)

S = slope (ft/ft)

n = Manning's roughness

I<sub>i</sub> = rainfall intensity

C = rational runoff coefficient

A	B	C	D	E	F	G	H	I	J	K	L	M	N	O
1	Watershed Basin Number	A		Solving for Time of Concentration										
2	Total Drainage Area	45		Kinematic Wave Theory										
3	Rational Method for Flow	RUNOFF COEFFICIENT		User Data										
4	Subarea A (acres)	30		Calculated Value										
5	Subarea A Runoff Coefficient	0.6	LAND USE	Length of overland flow	50,000	feet	Surface	Smooth Surface	Surface Mannings n					
6				Mannings "n" for surface	0.800		Base Earth							0.011
7	Subarea B (acres)	15	BUSINESS	Average watershed slope	0.080	ft./ft.	Fallow							0.050
8	Subarea B Runoff Coefficient	0.25	DOWNTOWN AREAS	Constant alpha	0.527		Cultivated, <= 20% Residue							0.060
9	Subarea C (acres)		NEIGHBORHOOD AREAS	Constant n	1.667		Cultivated > 20% Residue							0.170
10	Subarea C Runoff Coefficient			Weighted Runoff Coefficient	0.48		Grass, Short							0.150
11	Subarea D (acres)		SINGLE FAMILY AREAS				Grass, Dense							0.240
12	Subarea D Runoff Coefficient		MULTI UNITS, DETACHED				Grass, Bermuda							0.410
13	Weighted Runoff Coefficient	0.4833	MULTI UNITS, ATTACHED				Woods, Light							0.400
14	2-year Rainfall Intensity (IDF)	3.83	SUBURBAN				Woods, Dense							0.800
15	10-year Rainfall Intensity (IDF)	8.96												
16	Q2 Flow	83.3	INDUSTRIAL:	Trail Time of Duration			Rainfall Intensity(IDF)							
17	Q10 Flow	110.1	LIGHT AREAS	Tc (minutes)			Calculation of Time of Concentration							
18			HEAVY AREAS											
19			PARKS, CEMETARIES											
20			PLAYGROUNDS											
21			RAILROAD YARD AREAS											
22			UNIMPROVED AREAS											
23			STREETS:											
24			ASPHALT	0.7-0.95										
25			CONCRETE	0.8-0.95										
26			BRICK	0.7-0.85										
27			DRIVES AND WALKS	0.75-0.85										
28			ROOFS	0.75-0.85										
29			LAWNS:											
30			SANDY SOIL, FLAT, 2%	0.05-0.1										
31			SANDY SOIL, AVE, 2-7%	0.1-0.15										
32			SANDY SOIL, STEEP, 7%	0.15-0.2										
33														
34														
35			HEAVY SOIL, FLAT, 2%	0.13-0.17										
36			HEAVY SOIL, AVE, 2-7%	0.18-0.22										
37			HEAVY SOIL, STEEP, 7%	0.25-0.35										
38			AGRICULTURAL LAND:											
39			BARE PACKED SOIL											
40			SMOOTH	0.3-0.6										
41			ROUGH	0.2-0.5										
42			CULTIVATED ROWS											
43			HEAVY SOIL, NO CROP	0.3-0.6										
44			HEAVY SOIL, WITH CROP	0.2-0.5										
45			SANDY SOIL, NO CROP	0.2-0.4										
46			SANDY SOIL, WITH CROP	0.1-0.25										
47			PASTURE											
48			HEAVY SOIL	0.15-0.45										
49			SANDY SOIL	0.05-0.25										
50			WOODLANDS	0.05-0.25										
51														
52	Revised 11/25/2008	TGH												
53														

# STORM DURATION

By setting the storm duration equal to the time of concentration, you are producing a storm event with the maximum peak discharge.

Q: Why did you set the storm duration greater than the time of concentration?

A: You want to make sure that all of the drainage area is contributing.

$$T_c = 15.5 \text{ min.}$$

Boone, North Carolina 36.2167N, 81.6667W											
ARI* (years)	5 min.	10 min.	15 min.	30 min.	60 min.	120 min.	3 hr.	6 hr.	12 hr.	24 hr.	
2	5.71	4.57	3.83	2.64	1.66	1.00	0.72	0.48	0.31	0.18	
10	7.50	6.00	5.06	3.67	2.39	1.46	1.06	0.69	0.44	0.28	
25	8.59	6.85	5.78	4.28	2.85	1.77	1.29	0.83	0.52	0.34	
100	10.38	8.25	6.95	5.32	3.67	2.35	1.72	1.08	0.65	0.44	

<http://portal.ncdenr.org/web/lr/links>

The screenshot shows a web browser window displaying the NC DENR Links page. The page is titled "Engineering Design Downloads" and "Design Calculation Spreadsheets". The left sidebar contains a navigation menu with categories like "Sedimentation and Erosion Control for Lots", "Sedimentation Control", "Commission", "Trout Buffer Requirements", "October 2010", "N.C. Geological Survey", and "Commissions".

**Engineering Design Downloads**

- Natural Resources Conservation Services (NRCS) Hydraulics and Hydrology Tools and Models - Win TR-55
- Natural Resources Conservation Services (NRCS) Revised Universal Soil Loss Equation, Version 2
- Natural Resources Conservation Services (NRCS) - Conservation Engineering Tools and Documents
- Natural Resources Conservation Services (NRCS) - Stream Corridor Restoration
- Federal Highway Administration
- North Carolina Department of Transportation - Erosion and Sediment Control Measures
- North Carolina Department of Transportation - Roadway Standard Drawings Library
- Maine DOT charts for embedded culverts - Fish Passage Policy & Design Guide (2nd edition / December 2004) Click here for pdf file.

**Design Calculation Spreadsheets**

- Sediment Control Measures with Skimmer Dewatering Calculation 14 May 2013
- Sediment basin design (MS Excel)
- Rational Method with Kinematic Wave Tc - 20081125 (MS Excel)
- Rational method (MS Excel)
- Manning's "n" (MS Excel)
- Spillway capacity (MS Excel)
- Riprap outlet protection (MS Excel)
- NY riprap outlet protection (MS Excel)
- Plunge pool, submerged outlet (MS Excel)
- Plunge pool, cantilevered outlet (MS Excel)
  - Design Note 6: Riprap Lined Plunge Pool for Cantilevered Outlet (PDF)
- Open Channel Flow (all following are MS Excel)
  - Permissible velocity - vegetation
  - Tractive force - synthetic liner
  - Tractive force - riprap (mild slope)
  - Tractive force - riprap (steep slope)

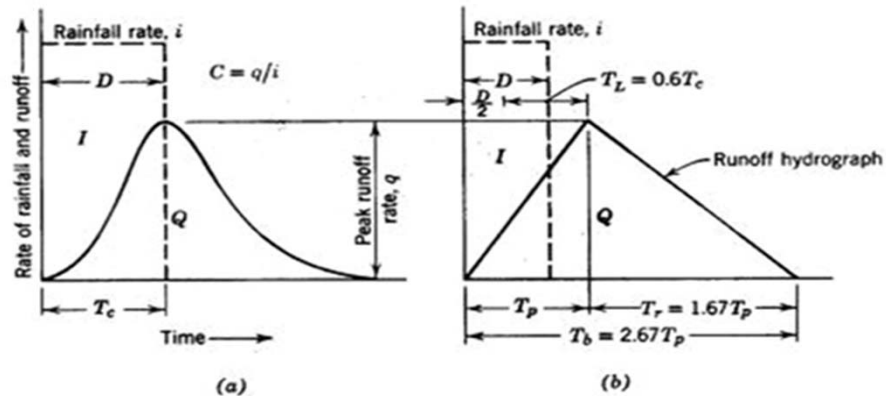
## ESTIMATING PEAK FLOW

- RATIONAL EQUATION,  $Q = CIA$
- $C = 0.48$
- $I = 5.06 \text{ in/hr}$
- $A = 45 \text{ Acres}$
- $Q = 109 \text{ cfs}$

## SCS TRIANGULAR HYDROGRAPH METHOD

- Step 1. Solve for Peak Flow and time to peak
- Step 2. Apply values to the SCS Triangular unit Hydrograph
- Step 3. Find the area of the triangle! ( $.5 * \text{Base} * \text{Heights}$ )

## SCS TRIANGULAR HYDROGRAPH

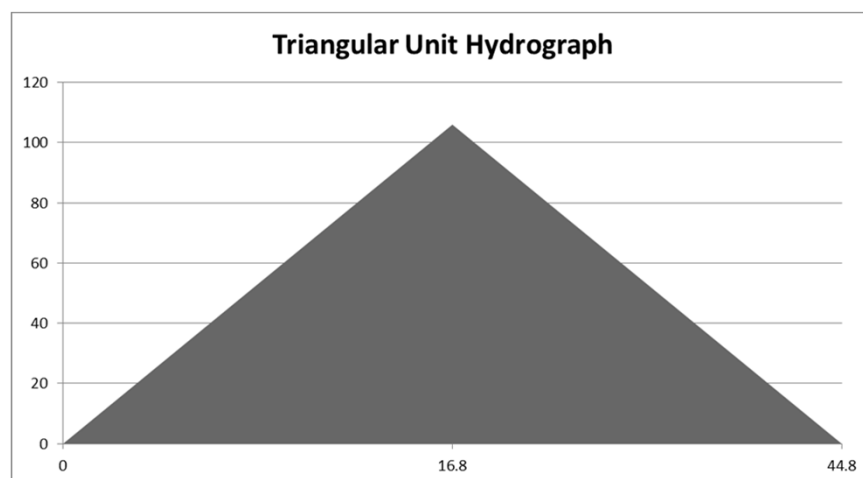




## Time to Peak, Time of Base

- Lag Time ( $T_L$ ) =  $T_C * 0.6$  (SCS Empirical Equation)
- Time to Peak ( $T_P$ ) =  $D/2 + T_L$
- $T_P = D/2 + T_C * 0.6$
- $T_P = (15/2) + (15.5 * 0.6) = 16.8$  Minutes
  
- Time of Base ( $T_R$ ) =  $1.67 * T_P$
- $T_R = 1.67 * 16.8 = 28$  Minutes

## AREA UNDER THE TRIANGLE



## RUNOFF VOLUME

- Solving for the area under the triangles!

$$(0.5 * 106 * 16.8 * 60) + (0.5 * 106 * 28 * 60)$$

$$53,424 + 89,040 = 142,464 \text{ Cubic Feet of Runoff!}$$

$$\text{Also, Volume} = 3.3 \text{ Acre-Feet}$$

## WHY IS THE VOLUME SO DIFFERENT?

- Volume 24 hr event = 14.4 Acre-Feet
- Volume 15 min. event = 3.3 Acre-Feet
- Peak Flow 24 hr event = 204
- Peak Flow 15 min. event = 106

From a depth perspective!

<b>Boone, North Carolina 36.2167N, 81.6667W</b>										
ARI* (years)	5 min.	10 min.	15 min.	30 min.	60 min.	120 min.	3 hr.	6 hr.	12 hr.	24 hr.
2	0.48	0.76	0.96	1.32	1.66	2.00	2.18	2.85	3.77	4.39
10	0.62	1.00	1.26	1.83	2.39	2.92	3.18	4.10	5.28	6.61
25	0.72	1.14	1.45	2.14	2.85	3.55	3.87	4.94	6.21	8.07
100	0.86	1.38	1.74	2.66	3.67	4.69	5.15	6.47	7.82	10.65

## Why Runoff Volume?

- Sediment traps and basins are using total runoff volume and peak discharge rate.
- Designing with Peak discharge does not account for increased amounts of volume. This leads to traps and basins being over topped!
- Is a type II storm distribution unreasonable for sediment trap and basin design?